



<u>Environmental Application of Ashra</u> <u>Telescope - Imaging Lidar</u>

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Application to environmental monitoring

Lidar technology

Wide FOV, highresolution teles<u>cope</u>, Real-time monitoring of air pollution

Imaging Lidar

Targets:

Suspended particulate matter(SPM); car emissionWind speed and direction

•Volcanic SO₂

e.g. Eruption of Miyake-jima island Advection of highly concentrated SO_2 SO₂ from Miyake-jima (simulation)



2001/04/01/22 JST

Imaging vs. conventional lidar measurement

Conventional system (narrow FOV)

?Time and labor consuming for scanning operations? Normally time-height indication is employed for vertical measurement



Scanning

FOV of imaging lidar

FOV of conventional lidar



Imaging lidar Wide FOV (50 ° × 50 °): fixed direction Scanning laser beam Real-time measurement of aerosol distribution

Aerosols



CEReS Project 3 **Evaluation of radiation budget and long-term changes of atmospheric parameters using satellite and ground observation network data**



Radiative forcing: large error bars for aerosols and clouds



Source: IPCC (2001)

Long-term aerosol sampling in Chiba (1998-2004)

Fukagawa et al., Atmospheric Environment, 40, 2160 (2006)



Aerosol characteristics over the urban Chiba area



Aerosol size distribution



Wavelength dependence of aerosol extinction coefficients



0.1 1 10 Wavelength (um) **TIDDAN**

Phase functions (Angular dependence of the differential cross-section)



Non-spherical particles

Prolate Spheroid, = 0.55μ m, r = 1.0μ m, n' = 1.53 - 0.008i



Lidar detection of aerosol particles

1/3 scale model Ashra telescope **Bistatic measurement** ? Both nighttime and daytime Range: 100 m - 3 km ? **Monostatic (backscattering)** measurement

Application: road-side measurement of SPM





Eye-safety

Laser power must be under the Maximum Permissible Exposure (MPE) (JIS C6802 safety standard)

• Operation wavelength of the Ashra telescope is between 300-420 nm.

(Wavelength range of the air-shower fluorescence)

- For a pulse width of 20 ns with 2 kHz repetition frequency,
 - MPE = $4 J/m^2 @ 355 nm$

(about 300 μ J/pulse for a beam diameter of 10 mm) *cf.* MPE = 5 mJ/m² [@] 532 nm

Rayleigh and Mie scattering patterns



Theory of Mie scattering



$$\boldsymbol{p}_{l}(\cos\boldsymbol{q}) = \frac{1}{\sin\boldsymbol{q}} P_{l}^{(1)}(\cos\boldsymbol{q}) , \quad \boldsymbol{t}_{l}(\cos\boldsymbol{q}) = \frac{d}{d\boldsymbol{q}} P_{l}^{(1)}(\cos\boldsymbol{q})$$
Associated Legendre functions

Constants determined by the boundary conditions: (a_l, b_l)

$$a_{l} = \frac{\mathbf{y}_{l}'(\widetilde{n}ka)\mathbf{y}_{l}(ka) - \widetilde{n}\mathbf{y}_{l}(\widetilde{n}ka)\mathbf{y}_{l}'(ka)}{\mathbf{y}_{l}'(\widetilde{n}ka)\mathbf{V}_{l}(ka) - \widetilde{n}\mathbf{y}_{l}(\widetilde{n}ka)\mathbf{V}_{l}'(ka)}$$

 $b_{l} = \frac{\widetilde{n} \mathbf{y}_{l}'(\widetilde{n} ka) \mathbf{y}_{l}(ka) - \mathbf{y}_{l}(\widetilde{n} ka) \mathbf{y}_{l}'(ka)}{\widetilde{n} \mathbf{y}_{l}'(\widetilde{n} ka) \mathbf{V}_{l}(ka) - \mathbf{y}_{l}(\widetilde{n} ka) \mathbf{V}_{l}'(ka)}$

 \widetilde{n} complex refractive index

k=2p/l

a radius of the dielectric sphere

$$\begin{cases} \mathbf{y}_{l}(\mathbf{x}) = (-1)^{l} \mathbf{x}^{l+1} \left(\frac{1}{\mathbf{x}} \frac{d}{d\mathbf{x}} \right)^{l} \left(\frac{\sin \mathbf{x}}{\mathbf{x}} \right) \\ \mathbf{c}_{l}(\mathbf{x}) = (-1)^{l} \mathbf{x}^{l+1} \left(\frac{1}{\mathbf{x}} \frac{d}{d\mathbf{x}} \right)^{l} \left(\frac{\cos \mathbf{x}}{\mathbf{x}} \right) \\ \mathbf{V}_{n}(\mathbf{x}) = \mathbf{y}_{l}(\mathbf{x}) + i \mathbf{c}_{l}(\mathbf{x}) \end{cases}$$



Aerosol measurement using CEReS 4wavelength lidar

•355, 532, 756, and 1064 nm

80 cm telescope with4 photomultipliers

Kinjo *et al.*, Jpn.J. Appl.Phys., 40, 434-440 (2001)

Yabuki *et al.* Jpn.J.Appl.Phys., 42, 686-694 (2003).



Lidar equation (elastic backscattering)



- *c* light speed [m/s] laser pulse duration [s]
- A telescope area [m²]
- K optical efficiency
- $G\left(R
 ight) \,\,$ overlapping function

Solution of lidar equation (Fernald method)

$$S_{1}(R) = \mathbf{a}_{1}(R) / \mathbf{b}_{1}(R) = \mathbf{s}_{1}(R) / \left(\frac{d\mathbf{s}_{1}}{d\Omega}\right)_{q=p}, \quad S_{2}(R) = \mathbf{a}_{2}(R) / \mathbf{b}_{2}(R) = 8.52$$

$$\boldsymbol{a}_{1}(R) = -\frac{S_{1}(R)}{S_{2}} \boldsymbol{a}_{2}(R) + \frac{S_{1}(R) X(R) \exp I(R)}{\frac{X(R_{c})}{\frac{A_{1}(R_{c})}{S_{1}(R_{c})} + \frac{A_{2}(R_{c})}{S_{2}}} + J(R)$$

$$X(R) = R^{2}P(R), \quad I(R) = 2\int_{R}^{R_{c}} \left[\frac{S_{1}(R')}{S_{2}} - 1\right] a_{2}(R') dR'$$
$$J(R) = 2\int_{R}^{R_{c}} S_{1}(R') X(R') \exp I(R') dR'$$

Aerosol extinction profile $a_1(z, l, S_1)$



 $a_1(z, l) = N(z)s_1(l)$ N:number density s_1 :total cross section

Extinction profile varies when calculated with different S_1 parameter. (The same lidar data leads to different transmittance.)

Raw and range-squared signals



Simulation of the signal-to-noise ratio





Lidar equation for bistatic measurement

$$P = P_0 K \frac{A}{r^2} ds \boldsymbol{b}(\boldsymbol{q}_{scat}) T_t T_r$$

where $ds = \frac{r \boldsymbol{q}_{\text{FOV}}}{\sin(\boldsymbol{q}_{\text{scat}})}$

- P Received power [W]
- P_0 Transmitted power [W]
- *K* Optical efficiency of the telescope
- *A* Effective area of main mirror [m²]
- *r* Range to the target [m]
- *ds* Laser path length in one pixel [m] Scattering coefficient [m⁻¹sr⁻¹]
- $T_{\rm t}$ Transmittance from laser to target
- $T_{\rm r}$ Transmittance from target to telescope



Model profile of the atmosphere



Signal-to-Noise Ratio



Measurement of atmospheric transmittance

Signal & laser @ site 1

$$P_{11} = P_0^{(1)} K^{(1)} \frac{A_1}{r_1^2} dr_1 \boldsymbol{b} (\boldsymbol{p}) T_1^2$$

Signal & laser @ site 2

$$P_{22} = P_0^{(2)} K^{(2)} \frac{A_2}{r_2^2} dr_2 \mathbf{b}(\mathbf{p}) T_2^2$$

Signal @ site 1 (laser @ site 2)

$$P_{12} = P_0^{(2)} K^{(1)} \frac{A_1}{r_1^2} ds_1 \boldsymbol{b} (\boldsymbol{q}_{\text{scat}}) T_1 T_2,$$

$$ds_1 = \frac{r_1 \boldsymbol{q}_{\text{FOV}}^{(1)}}{\sin \boldsymbol{q}_{\text{scat}}}$$

 $ds_2 =$

Signal @ site 2 (laser @ site 1)

$$P_{21} = P_0^{(1)} K^{(2)} \frac{A_2}{r_2^2} ds_2 \mathbf{b} (\mathbf{q}_{\text{scat}}) T_1 T_2 ,$$



Solution of the coupled equations

$$Q_{11} = \boldsymbol{b} (\boldsymbol{p}) T_1^{2}$$

$$Q_{22} = \boldsymbol{b} (\boldsymbol{p}) T_2^{2}$$

$$Q_{12} = Q_{21} = \beta(\theta_{\text{scat}}) T_1 T_2$$

b(**p**): backscattering coefficient

 T_1, T_2 : transmittance

$$Q_{12} = Q_{21} = \beta(\theta_{\text{scat}})T_1T_2$$

$$\frac{\beta(\pi)}{\beta(\theta_{\text{scat}})} = \frac{(Q_{11}Q_{22})^{1/2}}{Q_{12}} , \quad T_2^2 = \frac{Q_{22}}{Q_{11}}T_1^2$$

... General solution for non-homogeneous atmosphere

Solutions for the layered atmosphere

$$T_{0}(z) = \exp\left[-t_{0}(z)\right]$$

$$= \exp\left[-\int_{0}^{z} a(z')dz'\right]$$

$$T_{0}$$

$$T_{1}$$

$$T_{1} = \exp\left[-\frac{t_{0}(z)}{\sin q_{1}}\right], \quad T_{2} = \exp\left[-\frac{t_{0}(z)}{\sin q_{2}}\right]$$

$$\sin q_{1} \ln T_{1} = \sin q_{2} \ln T_{2}, \quad T_{1} = \exp\left[\frac{\ln(\frac{Q_{22}}{Q_{11}})}{2\left(\frac{\sin q_{1}}{\sin q_{2}}-1\right)}\right]$$

Iterative analysis of bistatic lidar data





Imaging lidar









CEReS Observatory for Ashra Imaging Lidar















Photonics Industries DC-30-351SP 351 nm, Nd:YLF laser 300 mW @ 3 kHz (100 uJ/pulse) 10-25 ns, 0-10 kHz





<u>CCD cameras</u>



Cooled CCD SBIG ST7 765 \times 510 pixels QE 0.65 @ 532 nm 16 bit ADC Lens FOV 46 deg Aperture 25 mm Filter T=0.54 @ 530nm



Cooled CCD BITRAN 4008 × 2672 pixels QE 0.47 @ 532 nm, 16 bit ADC Lens (SIGMA) 50mm, f/1, 39 deg Filter T=0.54 @ 530 nm Half bandwidth =100 nm

Gate I.I. (C9547-03MOD) Gate time 10 ns –DC, max.rep. 10Hz 185-900 nm, 1 stage MCP Luminous gain 1×10^4 (lm/m²) $\frac{1}{3}x$



- ? Observation of very intense forward scattering
- ? Observation capability near the ground level
- ? Limited dynamic range for the detector

? Consideration for polarization, multiple-scattering, and phase function of aerosol particles

Imaging Lidar Observation (CCD camera)

05.01.26 @ ICF



Extraction of Laser path intensity

05.01.26 @ ICF



04/11/02_{laser} = 10 deg. Exposure time = 0.5 s

(a) Laser ON





Geometry of the in-plane observation

05.01.26 @ ICF



$$\frac{d\boldsymbol{s}}{d\Omega} = \left(\frac{\boldsymbol{\tilde{a}} \ k^2}{4\mathrm{pe}_0}\right)^2 \frac{\mathsf{S} \quad \mathsf{P}}{1 + \cos^2 ?}$$



Laser path intensity









Observed signal intensity







Imaging Lidar Observation – 351nm, In-plane



Imaging Lidar Observation – 532nm, Cross-plane

ross-plane observation

▲ Laser 250n CCD

Nd:YAG Laser, 532nm 10Hz, 100mJ/pulse

Continuous mode (without gating)

Gated mode Exposure time 2 s Gate width 250 ms



II I Image Internettion



S/N Improvement with GPS 1PPS

GPS trigger synchronization system

Trigger synchronization system (TSS) has been developed to improve S/N by applying the GPS 1 PPS (pulse-per-second) system. Gating operation of I.I. is synchronized to the laser pulse emission with the accuracy of approx. ± 1 m (gate time > a few tens of m).





Fast-Gate Image Intensifier UnitHAMAMATSU C9547-03MODGate time $10ns \sim DC$ Max. Gate Repetition rate 10kHzSize of Input/Output surface25mmWavelength range $185 \sim 900nm$ MCP1 stageLuminous gain $1.0 \times 10^4 \ (lm/m^2) \cdot k$

Accuracy of trigger synchronization



Image obtained with the gated I.I. + CCD

05.01.26 @ ICF



04/12/08 351 nm, 3 kHz 100 mJ/pulse Exposure time = 1.0 s

Gate mode (Gate time = a few ms)

S/N = 4.2 ()

S/N = 24.8 (

Environmental Ashra telescope

1/3-scale Ashra telescope



1/3 scale Ashra Telescope: configuration

Baker-Nunn optical system:

consisting of a spherical mirror with three correction lenses



Spherical mirror (60cm)

· Image Intensifier

1/3 scale Ashra Telescope: construction





lenses ◄

Detector

Adjustment of elevation angle







Modified Baker-Nunn optics



Electrostatic image intensifier



	Voltage (kV)
PC	0
G1	0.342
G2	1.527
G3	11.07
Α	30.3



6-inch image intensifier



ES I.I. Gate I.I. CCD camera

Test system for UV laser light detection

05.01.26 @ ICF

CCD



First observation of the UV laser beam



S/N = 136(@ X = 2256 px)

- **Detector: UV II + gate II + CCD Exposure: 1.0 s**
- Laser output: 60 mJ/pulse, 3 kHz Gate time = 5 ms



Observation of stars at CEReS site

2007/2/21 19:10 FOV= 42 deg, res=4.3 arcmin=1.3 mrad



Performance of the 1/3-scale models

Configuration of the measurement



Observed image of the UV laser beam





SN of UV laser beam observation

(a) Laser ON







Observation angle :31 °, Angular resolution :3. arcmin (1.1mrad) Laser output energy :10 mJ/pulse ,10 Hz Elevation angle :35 deg Exposure :1 s Gate I.I. Gain : 210 (lm/m²)/lx (Control voltage 7.0 V)

S/N = 24.1



Scanning measurement (1)



Scanning measurement (2)



2-dimensional distribution of scattered intensity

Summary for the imaging lidar project



In the Ashra-I project, EHE cosmic-ray particles will be measured using wide-FOV, high-resolution telescopes. The FOV of 50 deg, resolution of 1 arcmin (0.29 mrad), intelligent high-speed shutter, and 1 kHz repetition rate indicate that the system has superior quality also for the telescope of an imaging lidar. The overall amplification factor of the detection system is 10⁶, equivalent to that of a conventional PMT.

•At CEReS, we are developing a Mie-scattering imaging lidar for the two-dimensional detection of aerosol particles. After completing the assembly of the 1/3-scale Ashra telescope, we are checking the overall performance of the system.