

Status of CANGAROO-III 2nd telescope

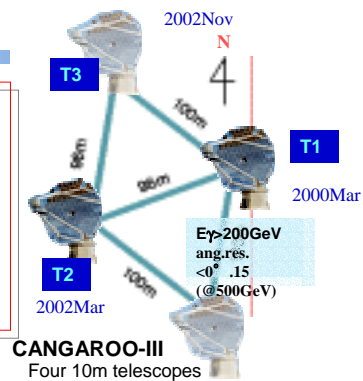
CANGAROO collaboration



CANGAROO-III project



Woomera, SA
 31° 06'S 137° 47'E
 160m a.s.l.
 Level plain
 desert climate
 CANGAROO
 experiment started in
 1992

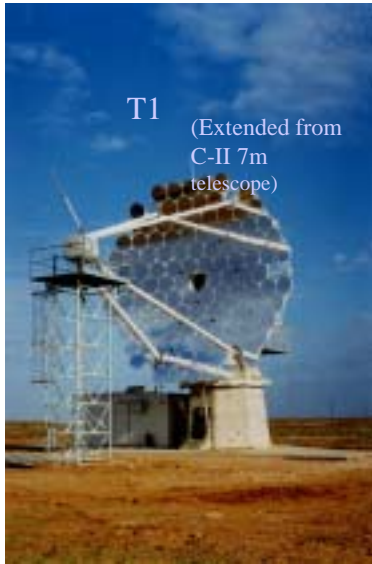


Construction schedule

- 2000.3 **T1**(C-III 1st telescope) completion
 (extension from the C-II 7m telescope)
- 2001 production of the 2nd telescope (**T2**)
- 2002.3 construction of **T3**

- 2002.11 tune-up of **T2**
 construction of the 3rd telescope(**T3**)
- .12 start stereo observation with **T1** & **T2**
- 2003 production of the 4th telescope(**T4**)
- 2003.4 construction of **T4**
 stereo observation with all 4 telescopes

CANGAROO-III telescope basic design



	T1	T2
Main mirror	Parabolic	
Mounting	Alt-azimuth	
Max tracking speed	0° .5 /sec	1° .0 /sec
Focal length	8m (F=0.8)	
# of mirrors	114	
Spot-size (FWHM)	0° .20	(~0° .15*)
FOV	3° .0	4° .2
Pixel size	0° .115	0° .168
# of PMTs	552	427
Readout electronics	TDC & ADC	

*estimation

Contents -improvement in the hardware of the 2nd telescope-

1.Optical reflector

- progress in the surface control of FRP mirror

2.PMT camera

- Wider Field Of View
- High Voltage control for individual PMT
- detailed pre-shipment calibration

3.Electronics ,data acquisition

- All VME-based modules
- Faster Data Acquisition
- Pattern trigger module

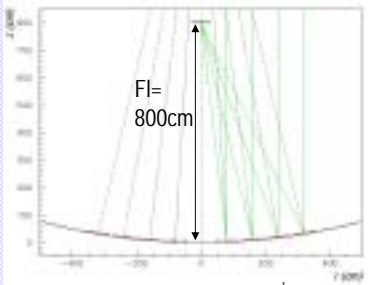
**CANGAROO-III
2nd telescope**

Optical reflector - design ,tessellated paraboloid-

Requirement for the reflector

- $\sim 0^\circ$.15 FWHM (-pixel size)
- High reflectance at 300-400nm

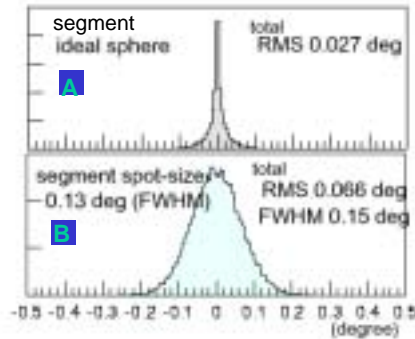
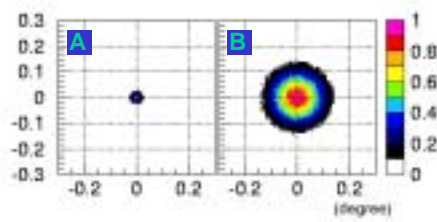
Spherical mirrors on paraboloid



$$CR(r) = \left\{ \left(fl - \frac{r^2}{4fl} \right)^2 + r^2 \right\}^{\frac{1}{2}} \times 2$$

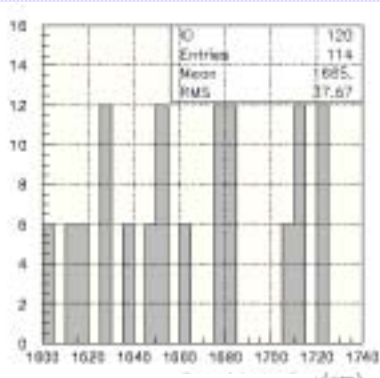
CR:16.0-17.2m
(16.6m as average)

Finite spot-size



Optical reflector – curvature radii-

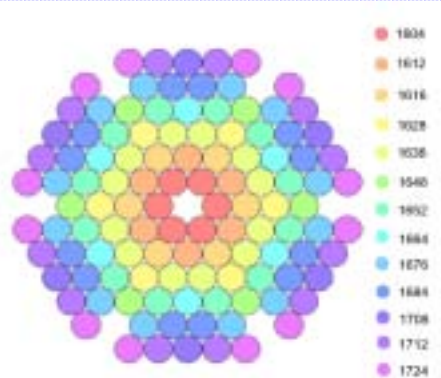
**Distribution of curvature radii
(design value)**



$$CR(r) = \left\{ \left(fl - \frac{r^2}{4fl} \right)^2 + r^2 \right\}^{\frac{1}{2}} \times 2$$

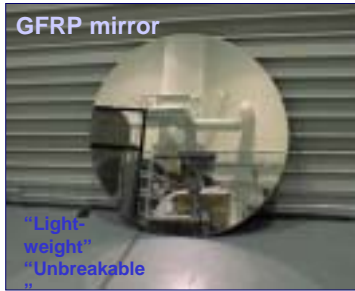
$$n(r)dr \propto r dr$$

**Position assignment on the
main mirror**

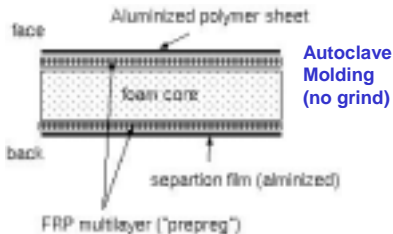


➤ Each mirror's position on the main mirror is assigned according to "resulted" curvature radius.

Optical reflector (1) -spherical mirror segments,design and formula-



Cross section of GFRP mirror



Material: CFRP → **GFRP**

(Glass Fiber Reinforced Plastic)

Diameter: 78cm

Weight: **5.6kg** + 1.1kg(back base)

Molding: vacuum bag + **autoclave**

Curvature radius: 16.0 ~ 17.2m

Spot size : $\sim 0^\circ .13$ in FWHM(typical)

Reflector metal : Aluminum

Surface protection: Fluoroplastic painting

Reflectivity: 80% @ 400nm

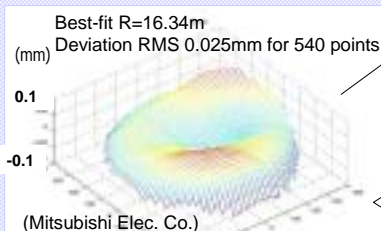
Alignment : tilt around 2 orthogonal axes
stepping motor control

Optical reflector (2) -small mirror segments,surface accuracy-

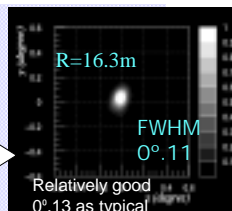
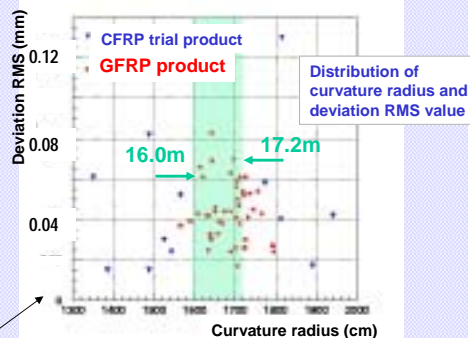
3D form measurement

➤ Surface height of the mirror is measured with 0.005mm accuracy for 540 points

➤ Two-parameters--"best-fit curvature radius" and "deviation from the sphere"-- are obtained.



3D form measurement data
-Deviation from ideal sphere-



Conventional
Spot-size test

➤ There seems to be some *progress* in the surface control .

➤ "typical" spot size of recently produced GFRP mirror is $0^\circ .13$ in FWHM with more than 80% acceptability.

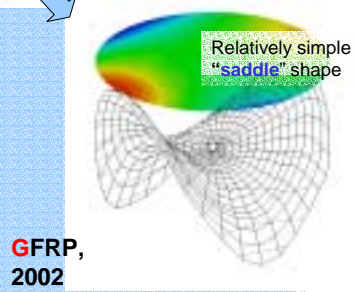
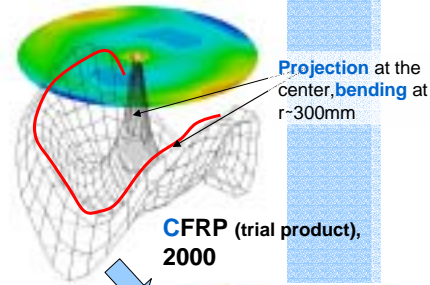
Optical reflector –FRP development-

Surface accuracy of FPR mirror is determined by the **balance of rigidity** of composite materials

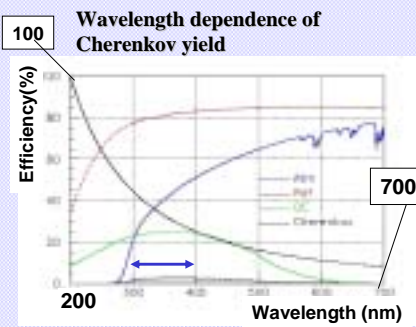
➤ **Recoil** of the core
 ⇕
 ➤ **Repression** of FRP sheets

- add/subtract components of multi-layer
- change layer thickness
- Change rigidity of material (core, FRP)etc.

Tendency of deformation

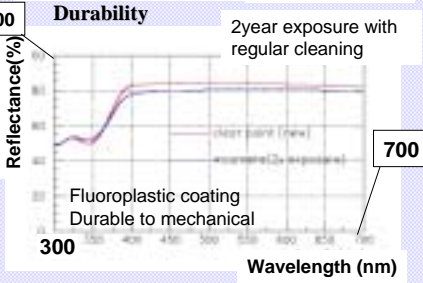
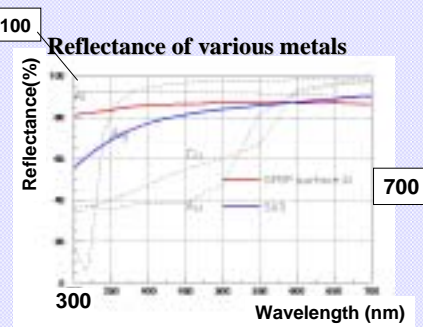


Optical reflector (3) -reflectance-



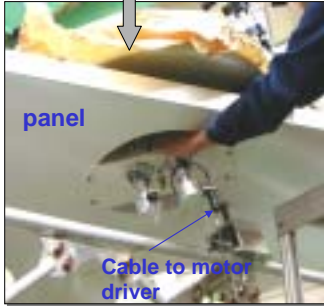
$$\text{Cherenkov yield} \propto \int_{\lambda_1}^{\lambda_2} \lambda^{-2} T(\lambda) \text{Ref}(\lambda) \text{QE}(\lambda) d\lambda$$

- **High reflectance** at shorter (300-400nm) waveband is required due to strong wavelength dependence of Cherenkov spectrum
- **Durability** under desert climate
- **Aluminum** (easily oxidized and corroded)+ surface protection



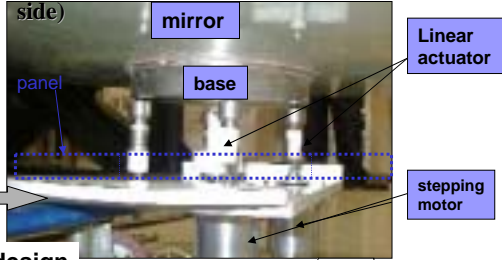
Optical reflector (4) –alignment system-

Axis alignment system



View from the back

Contact point(view from the side)



design

Tilt around 2 orthogonal axes
Resolution : 2.86×10^{-4} degree
Dynamic range: ± 2.86 degree

- Metal base is attached to the back surface of the mirror.
- The base is sustained by central screw clamp(fixed point) and 4 shafts.
- Two of them are linear actuator shaft whose length are controlled remotely using stepping motor.

test

- Smooth motion
- Repeatability
- Travel distance linearity

~0.02 alignment accuracy

Imaging camera (1) (2nd telescope)

S.Kabuki

Camera structure design

- Weight : **110kg**
- Hexagonal arrangement 427 PMTs
- Field of view : **4°** (0.168° /pixel)

PMT module design (427 PMTs)

- ¾ inch PMT(R3479,HPKK)
- +Preamp(MAX4107)

Light-guide design

- Winston cone shape
- Reflectance ~80 % (at 300~400nm)

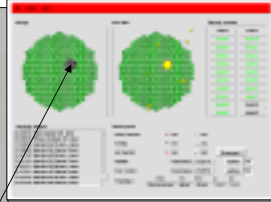
High Voltage supply

- GUI monitor program
- voltage controlled for individual PMT

New camera structure



PMT+Preamp assembly



Details are described in the poster by

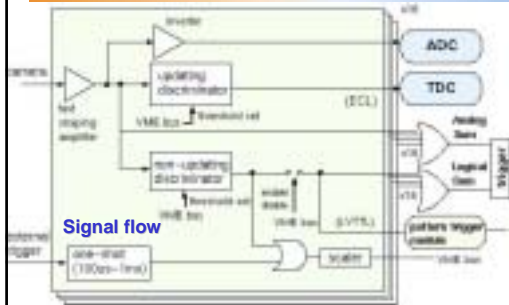
S.Kabuki (T09)

Light-guide

HV monitor program

HV off for bright stars

Electronics(1) front-end data acquisition



Custom-built VME-base front-end module



- **Lower threshold** means higher *trigger rate*, higher *deadtime ratio*
- shorter signal processing time—**faster data acquisition** is required for the observation with lower energy threshold.

VME-based modules

- Front-end Discriminator/scaler
- Charge ADC
16bit ADC chip for each channel
Readout time:10-20μsec/board
- TDC
1ns resolution

Acceptable trigger rate ~530Hz
(20% deadtime level)

Details are described in the poster by
D.Nishida (T17)

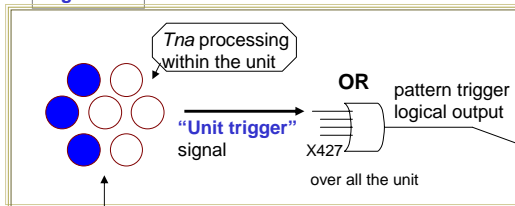
Electronics(2) Pattern trigger module

The second strategy to cope with *high trigger rate*

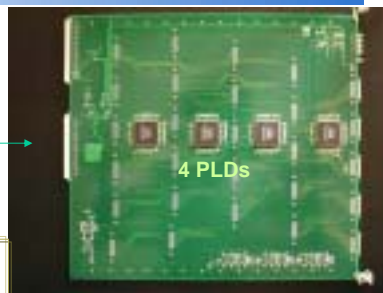
Suppress “junk” trigger at **online** level

Pattern trigger module using PLD
(Programmable Logic Device)

Algorithm



Transplant familiar “clustering” into hardware



Pattern trigger module(VME9U)
427channel input ,1ch NIM output

- **Pattern trigger(secondary)**
- **Normal trigger(primary)**

Details are described in the poster by
K.Nishijima (T18)

Current status of the 2nd telescope



summary

- The 2nd telescope of the CANGAROO-III project is now waiting tune-up for the operation.
- Hardware of the 2nd telescope is considerably improved.
- Tune-up of the 2nd telescope and construction of the 3rd telescope are both scheduled for November.



Test assembly of the 3rd telescope
(2002Aug, in Japan)